

Arm joint angle variability analysis in virtual robotic teleoperation with two master devices

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Introduction

- Teleoperated robotic systems are widely spreading in multiple fields: from telemedicine to radioactive materials handling.
- Users interact with a robot that acts as master device, controlling a slave manipulator that reproduce his/hers hand movements.
- While allowing for increased precision, tremor compensation, high dexterity and user comfort, teleoperation represents a complex motor control tasks that requires intensive training to master.
- This complexity comes from the kinematic redundancy that characterize the human arm: multiple joint configurations can be used to achieve the same hand movement.
- Previous works^[1] analyzed how novice and expert users were differently exploiting this redundancy to increase their performances in teleoperation using the Uncontrolled Manifold Analysis (UCM).

Goal

- In this work we propose the use of the UCM analysis as a way of assessing the differences between two different master devices in the motor control strategies adopted during the execution of different tasks.
- The UCM analysis allows for understanding how different master controller designs modify the way users coordinate the variability of their joint angles such that the ratio between variability that affects and that does not affect task performance is reduced.

Methods

Experimental Setup and UCM analysis



Fig. 1 - On the left, the three tasks developed; on the right, the user performs virtual teleoperation using the PL master device (Sigma.7). The arm and thorax movements are acquired with optical and electromagnetic markers

- The users performed 10 repetitions of 3 different tasks using a serial (SL) and a parallel link (PL) master device
 - Following an half-cloverleaf trajectory
 - Following an half-cloverleaf trajectory orienting the tool tip
- Reaching movements from a central position to eight targets
- Arm and thorax motions of eight right-handed users were acquired using electromagnetic and optical tracking devices.
- The joint angle vector (3) was computed through inverse kinematics using a seven-degrees-of-freedom musculoskeletal model in OpenSim^[2].
- Each repetition was **normalized in time** and the **mean joint angle** vector $\vec{\theta}$ was considered as the **reference** trajectory.

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- The arm Jacobian (J) was computed for each time sample.
 - The **deviations from the reference trajectories** were projected on the Jacobian null space and on its orthogonal matrix.

$$\theta_{TIM}(t) = \epsilon \epsilon^{T} \left(\theta(t) - \bar{\theta}(t) \right)$$

$$\theta_{TRM}(t) = \left(\theta(t) - \bar{\theta}(t) \right) - \theta_{TIM}(t)$$

where $\theta_{\text{TIM}}(t)$ represents the **task-irrelevant manifold**, ϵ is the null space of the Jacobian, and $\theta_{\text{TRM}}(t)$ represents the **task-relevant manifold**.

The variance per dimension of the norm of each projection was computed.

Preliminary results



Discussion

- The **preliminary results** obtained studying only **4 users** and the **first task**, show that **the components** of **variance**, for **both** master devices, are **not constant through** the **trajectory**.
- Following studies must take into consideration the different parts of the trajectory, with different curvatures and directions.

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References

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